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# پردازش سیگنال دیجیتال

درس ۲۰

## طراحی فیلترهای گسسته-زمان با پنجره‌زنی

Discrete-Time Filter Design by Windowing

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# Discrete-Time Filter Design by Windowing

# Filter Design by Windowing

- Simplest way of designing **FIR filters**
- Method is all **discrete-time** no continuous-time involved
- **Start** with ideal frequency response

$$H_d(e^{j\omega}) = \sum_{n=-\infty}^{\infty} h_d[n] e^{-j\omega n} \qquad h_d[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega$$

- Choose **ideal frequency response** as desired response
  - Most ideal impulse responses are of infinite length
- The easiest way to obtain a **causal FIR filter** from **ideal** is

$$h[n] = \begin{cases} h_d[n] & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$

- More generally

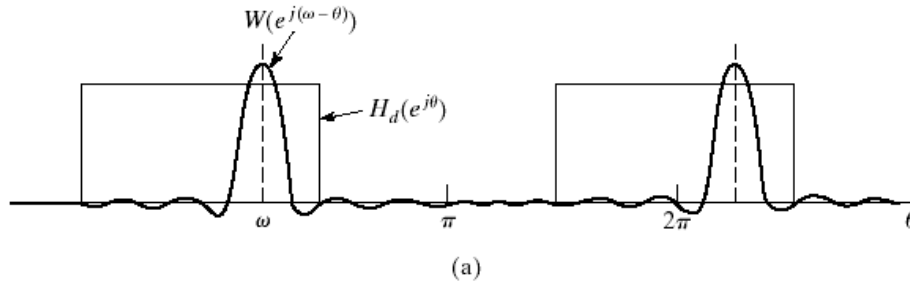
$$h[n] = h_d[n] w[n] \quad \text{where} \quad w[n] = \begin{cases} 1 & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$

# Windowing in Frequency Domain

- Windowed frequency response (Periodic Convolution)

$$H(e^{j\omega}) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\theta}) W(e^{j(\omega-\theta)}) d\theta$$

- The windowed version is smeared version of desired response



- If  $w[n] = 1$  for all  $n$ , then  $W(e^{j\omega})$  is impulse train with  $2\pi$  period (ideal case)

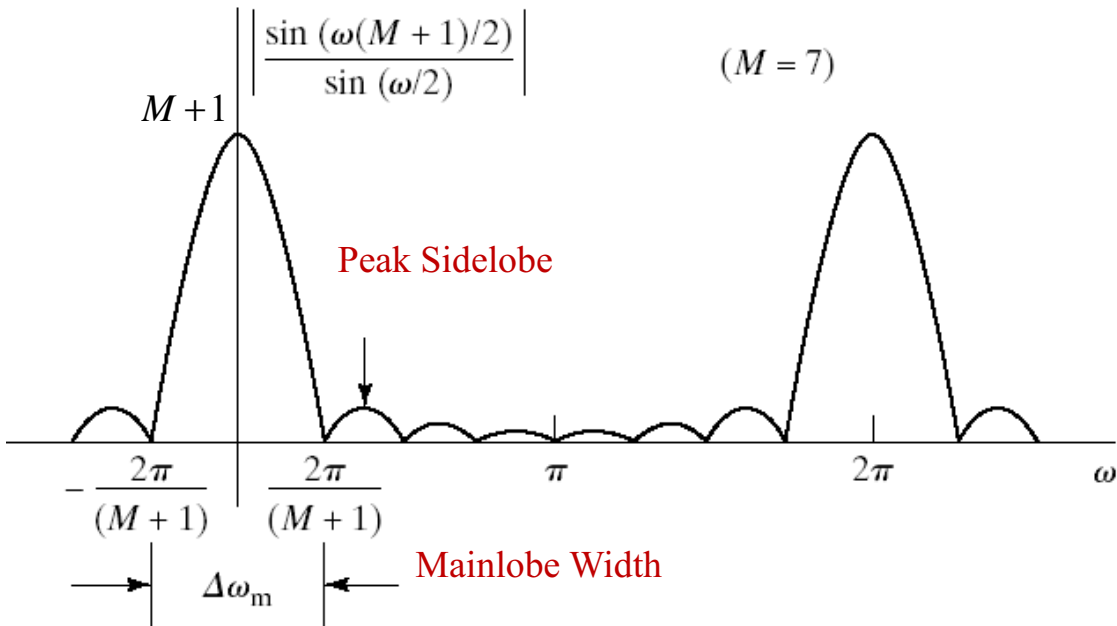
# Properties of Windows

- Prefer windows **that concentrate around DC** in frequency
  - (More similar to impulse  $\Rightarrow$ ) Less smearing, closer approximation
- Prefer window that has **minimal span in time**
  - Less coefficient in designed filter, **computationally efficient**
- **So we want concentration in time and in frequency**
  - *Contradictory requirements!*

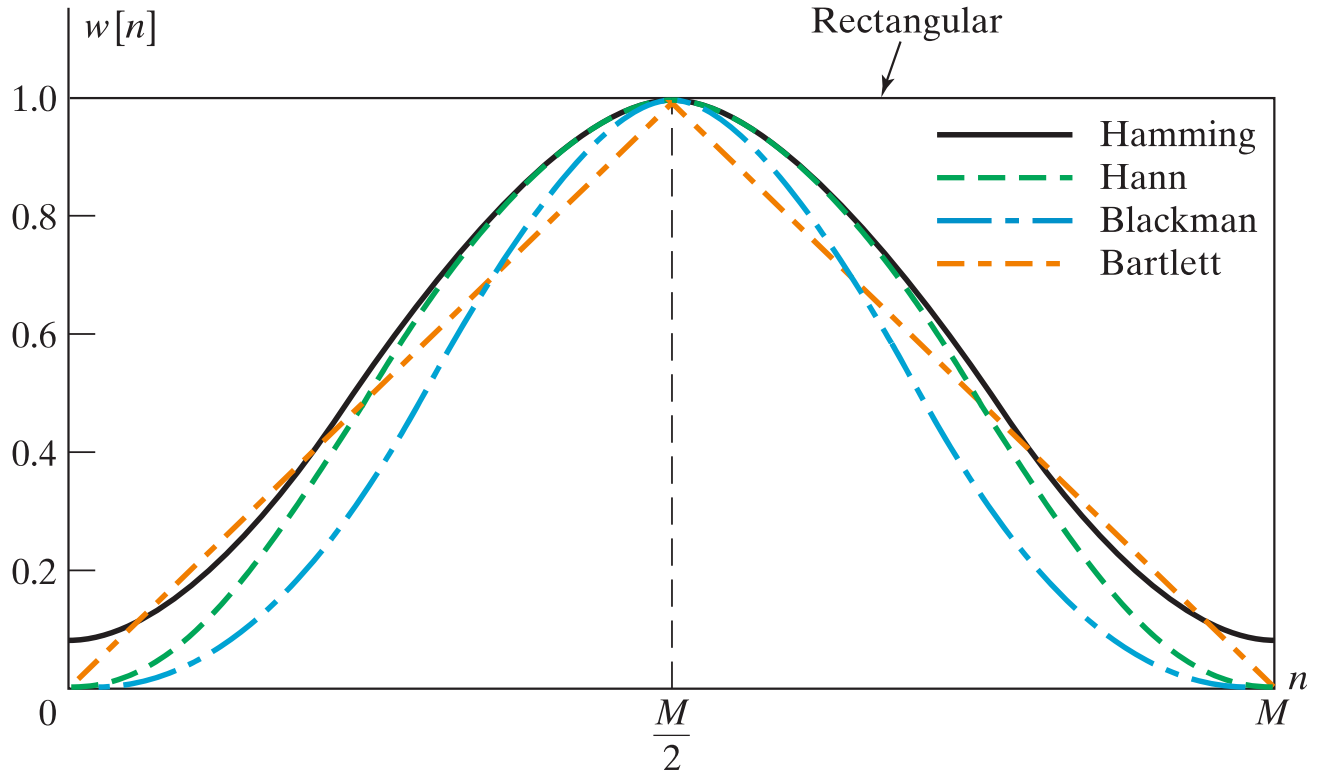
## Example: Rectangular window

- Example: Rectangular window

$$w[n] = \begin{cases} 1 & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases} \Rightarrow W(e^{j\omega}) = \sum_{n=0}^M e^{-j\omega n} = \frac{1 - e^{-j\omega(M+1)}}{1 - e^{-j\omega}} = e^{-j\omega M/2} \frac{\sin[\omega(M+1)/2]}{\sin[\omega/2]}$$



# Commonly Used Windows

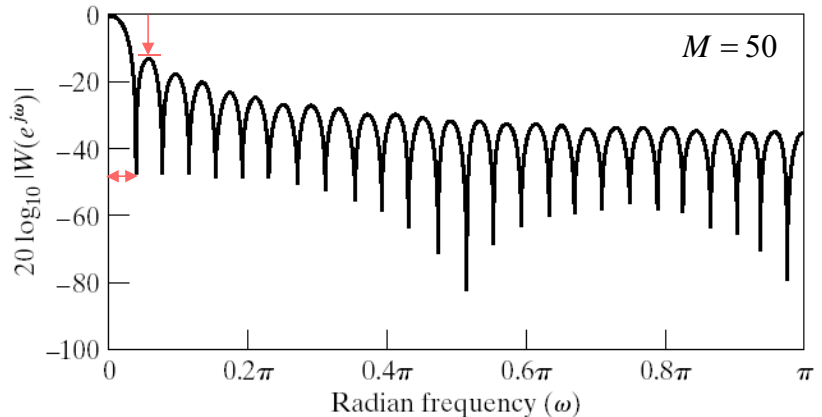
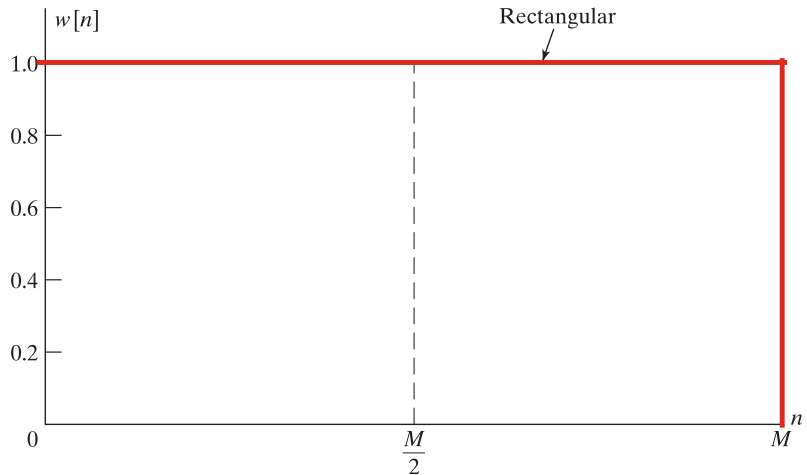


# Rectangular Window

- **Narrowest main lobe**
  - $4\pi/(M + 1)$
  - Sharpest transitions at discontinuities in frequency response  $H_d(e^{j\omega})$
- **Large side lobes**
  - $-13$  dB
  - Large oscillation around discontinuities

- **Simplest possible window**

$$w[n] = \begin{cases} 1 & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$





# Bartlett (Triangular) Window

- **Medium main lobe**

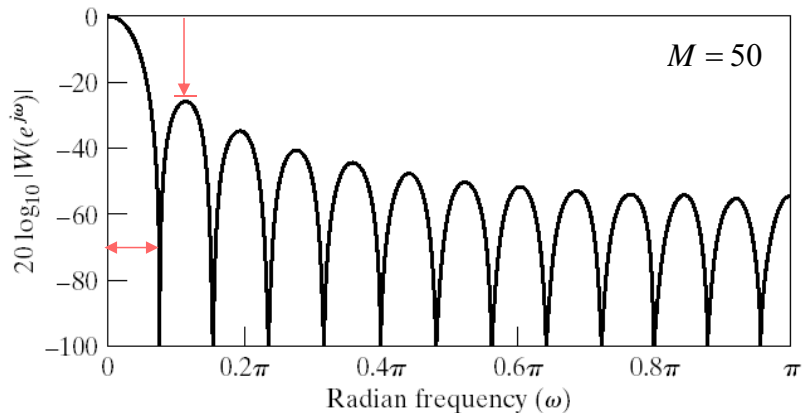
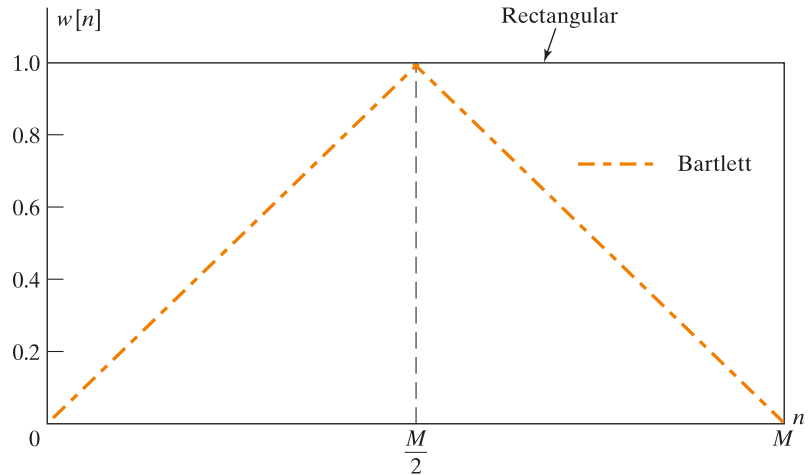
- $8\pi/M$

- **Side lobes**

- $-25$  dB

- Simple equation:

$$w[n] = \begin{cases} 2n/M & 0 \leq n \leq M/2 \\ 2 - 2n/M & M/2 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$



# Hanning Window (Hann)

- **Medium main lobe**

  - $8\pi/M$

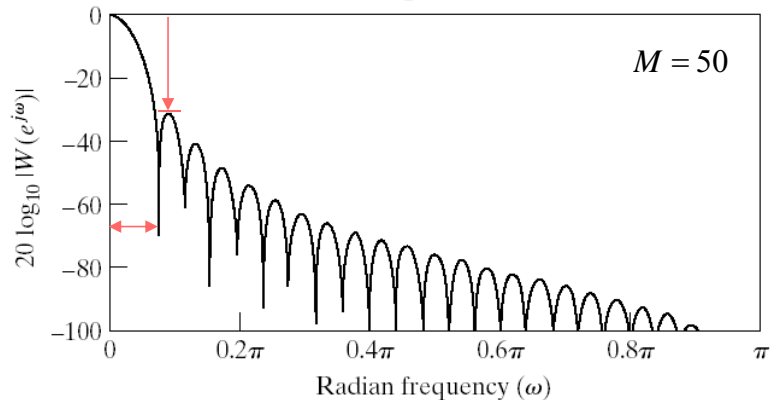
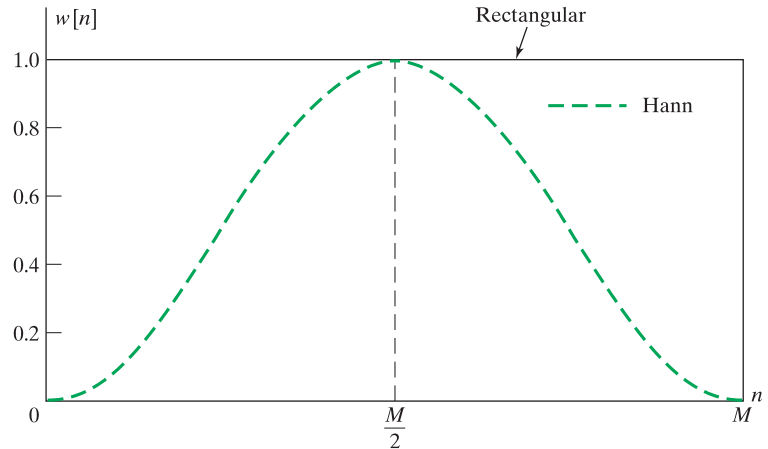
- **Side lobes**

  - $-31$  dB

- Hamming window performs better

- Same complexity as Hamming

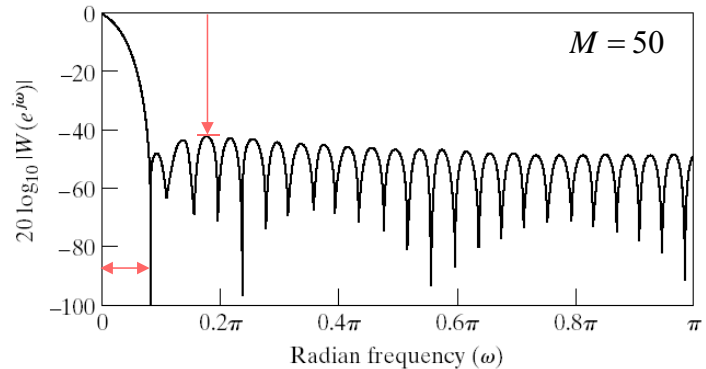
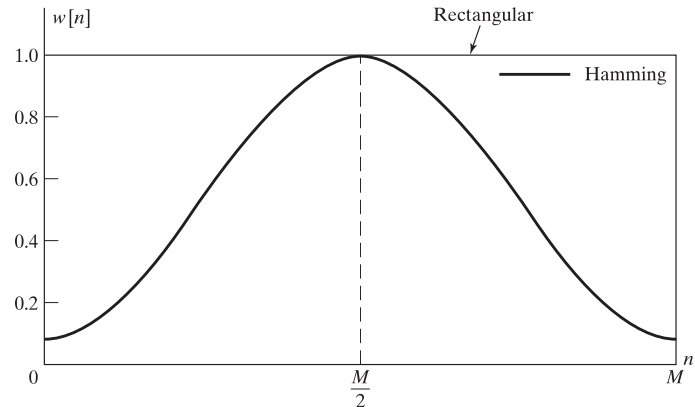
$$w[n] = \begin{cases} \frac{1}{2} \left[ 1 - \cos\left(\frac{2\pi n}{M}\right) \right] & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$



# Hamming Window

- **Medium main lobe**
  - $8\pi/M$
- **Good side lobes**
  - $-41$  dB
- Simpler than Blackman

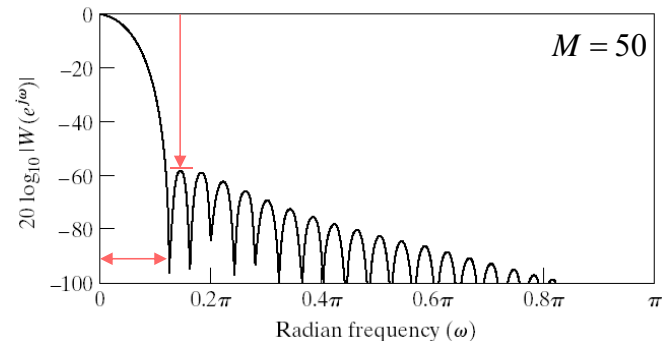
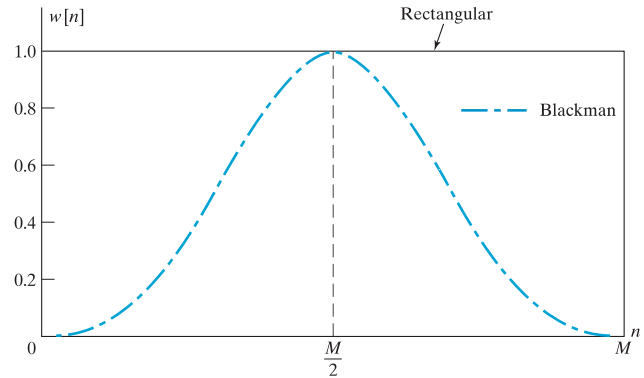
$$w[n] = \begin{cases} 0.54 - 0.46 \cos\left(\frac{2\pi n}{M}\right) & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$



# Blackman Window

- **Large main lobe**
  - $12\pi/M$
- **Very good side lobes**
  - $-57$  dB
- Complex equation

$$w[n] = \begin{cases} 0.42 - 0.5 \cos\left(\frac{2\pi n}{M}\right) + 0.08 \cos\left(\frac{4\pi n}{M}\right) & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$



# Incorporation of Generalized Linear Phase

- Windows are designed with **linear phase** in mind
  - Symmetric around  $M/2$

$$w[n] = \begin{cases} w[M-n] & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$

- So their Fourier transform are of the form

$$W(e^{j\omega}) = W_e(e^{j\omega}) e^{-j\omega M/2} \quad \text{where } W_e(e^{j\omega}) \text{ is a real and even}$$

- Will keep symmetry properties of the *desired impulse response*
- Assume symmetric desired response:

$$H_d(e^{j\omega}) = H_e(e^{j\omega}) e^{-j\omega M/2}$$

- With symmetric window

$$H(e^{j\omega}) = A_e(e^{j\omega}) e^{-j\omega M/2} \quad A_e(e^{j\omega}) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_e(e^{j\theta}) W_e(e^{j(\omega-\theta)}) d\theta$$

- Periodic convolution of real functions

# Linear-Phase Lowpass filter

- Desired frequency response  
(with generalized linear phase):

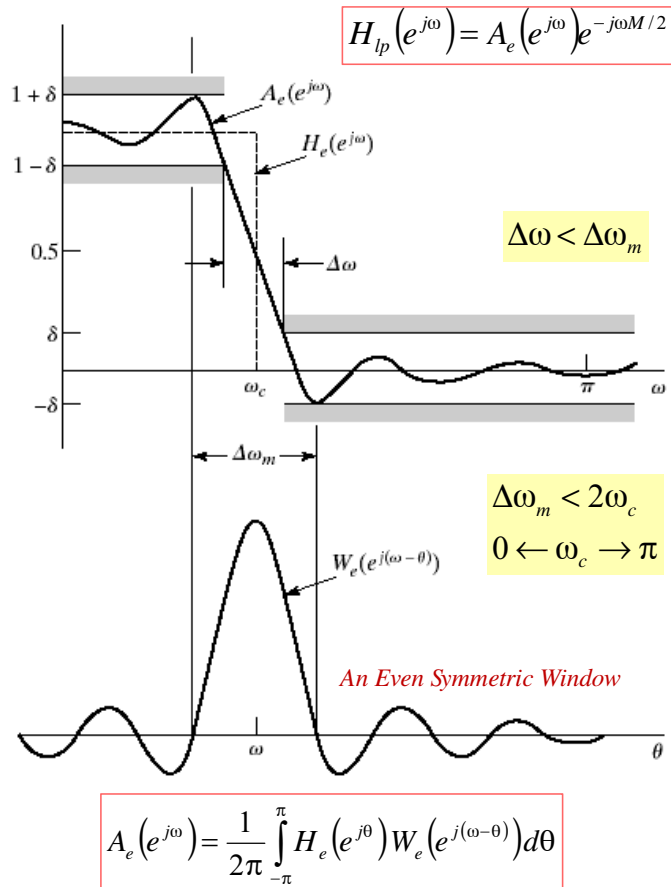
$$H_{lp}(e^{j\omega}) = \begin{cases} e^{-j\omega M/2} & |\omega| < \omega_c \\ 0 & \omega_c < |\omega| \leq \pi \end{cases}$$

- Corresponding impulse response  
(is also symmetric):

$$h_{lp}[n] = \frac{\sin[\omega_c(n - M/2)]}{\pi(n - M/2)}$$

- Desired response is **even symmetric**,  
use **symmetric window**

$$h[n] = \frac{\sin[\omega_c(n - M/2)]}{\pi(n - M/2)} w[n]$$

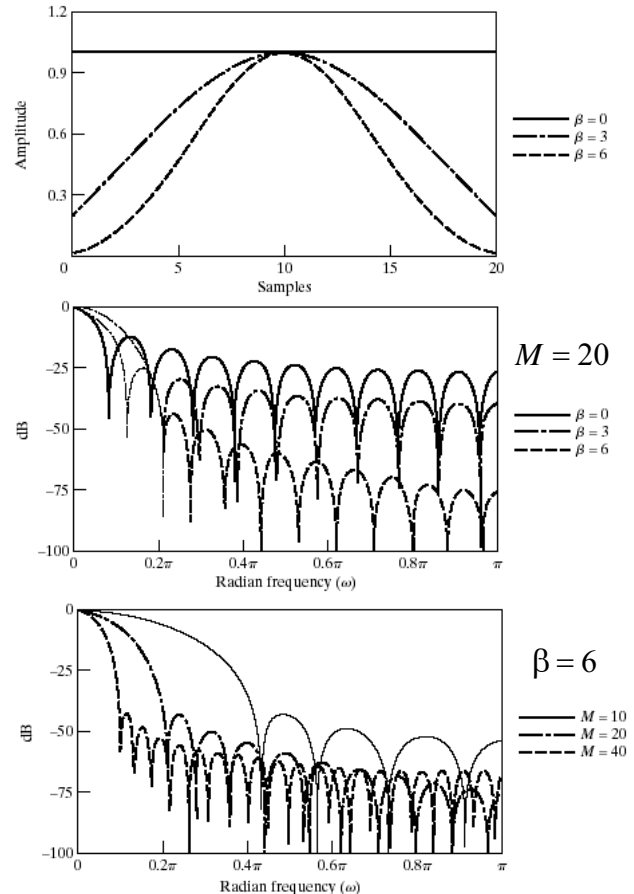


# Kaiser Window Filter Design Method

- Parameterized equation forming a set of windows
  - Has parameter to change **main-lobe width** and **side-lobe area trade-off**

$$w[n] = \begin{cases} \frac{I_0 \left( \beta \sqrt{1 - \left( \frac{n - M/2}{M/2} \right)^2} \right)}{I_0(\beta)} & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$

- $I_0(\cdot)$  represents **zeroth-order modified Bessel function of 1<sup>st</sup> kind**



## Determining Kaiser Window Parameters

- Given filter specifications Kaiser developed **empirical equations**
  - Given the peak approximation error  $\delta$  or in dB as  $A = -20\log_{10} \delta$
  - and **transition band width**  $\Delta\omega = \omega_s - \omega_p$
- The shape parameter  $\beta$  should be

$$\beta = \begin{cases} 0.1102(A - 8.7) & A > 50 \\ 0.5842(A - 21)^{0.4} + 0.07886(A - 21) & 21 \leq A \leq 50 \\ 0 & A < 21 \end{cases}$$

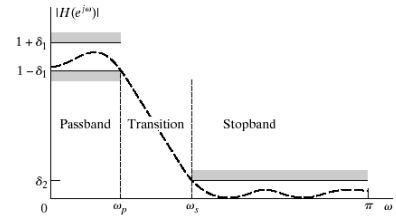
- The filter order  $M$  is determined approximately by

$$M = \frac{A - 8}{2.285\Delta\omega}$$



# Example: Kaiser Window Design of a Lowpass Filter

- Specifications  $\omega_p = 0.4\pi, \omega_s = 0.6\pi, \delta_1 = 0.01, \delta_2 = 0.001$
- Window design methods assume  $\delta_1 = \delta_2 = 0.001$
- Determine cut-off frequency
  - Due to the **symmetry** we can choose it to be  $\omega_c = 0.5\pi$



- Compute

$$\Delta\omega = \omega_s - \omega_p = 0.2\pi \quad A = -20 \log_{10} \delta = 60$$

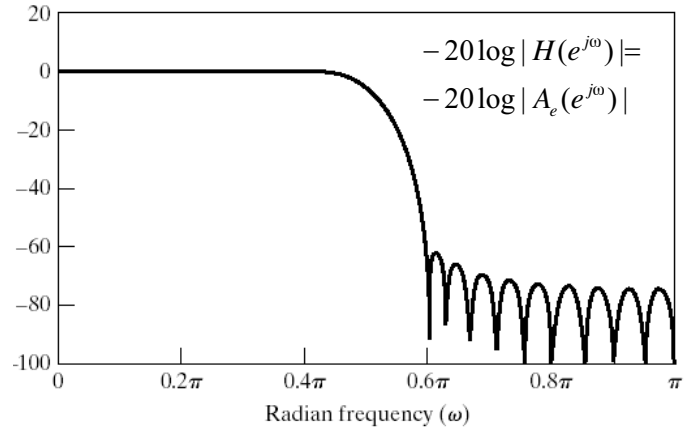
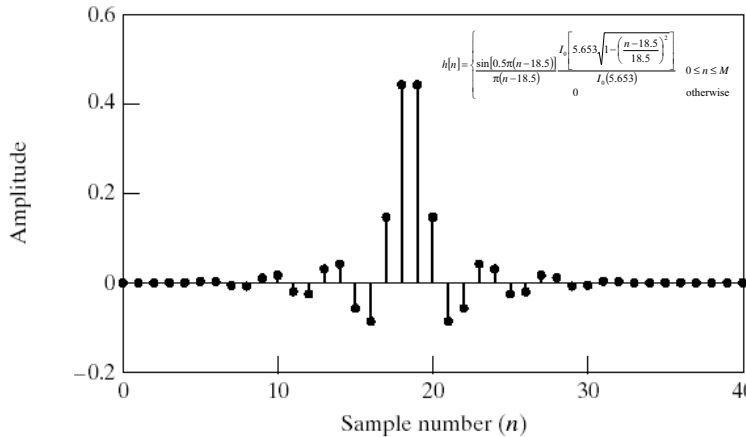
- And **Kaiser window** parameters

$$\beta = 5.653 \quad M = 37 \quad \text{Odd (Type II FIR with Lin. Phase)}$$

- Then the **impulse response** is given as

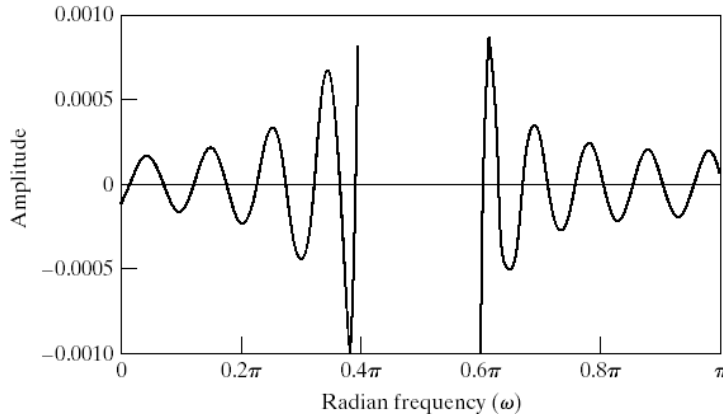
$$h[n] = \begin{cases} \frac{\sin[0.5\pi(n-18.5)]}{\pi(n-18.5)} \frac{I_0 \left[ 5.653 \sqrt{1 - \left( \frac{n-18.5}{18.5} \right)^2} \right]}{I_0(5.653)} & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$

# Example Cont'd



$M = 37$

Approximation Error



$$E_A(\omega) = \begin{cases} 1 - A_e(e^{j\omega}), & 0 \leq \omega \leq \omega_p, \\ 0 - A_e(e^{j\omega}), & \omega_s \leq \omega \leq \pi. \end{cases}$$

# General Frequency Selective Filters

- A general **multiband** impulse response can be written as

$$h_{mb}[n] = \sum_{k=1}^{N_{mb}} (G_k - G_{k+1}) \frac{\sin \omega_k (n - M/2)}{\pi(n - M/2)}$$

$$G_{N_{mb}+1} = 0$$

- Window methods can be applied to multiband filters
- Example multiband frequency response
  - Special cases of

- Bandpass
- Highpass
- Bandstop

